



A space imaging concept based on a 4m spun-cast borosilicate monolithic primary mirror (June 2010)

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4

Goals



- Create the largest monolith capable of being lifted in a DELTA VI or ATLAS V EELV to 500km LEO.
- Utilize existing technology for simplicity and rapid development.
- Use monolithic technology already demonstrated to be scalable to Ares V fairing sizes whose manufacturing is currently active.
 - Aim for complexity and areal density between HST and JWST.
 - Support a notional surveillance mission with a very large multiband push-broom instrument and heritage spacecraft for demonstration.
 - Provide wavefront control that rarely interrupts mission
 - Continuous NIIRS 7+ imaging
 - Stiff primary mirror supports 1g pre-flight testing with e.g., the LOTIS 6.5m Collimator.
 - Assess feasibility of using a cast borosilicate primary mirror in space.





University of Arizona, Steward Observatory Capabilities



 Devoted more than 25 years to casting, polishing, and testing very large, fast (~f/1.2) aspheric borosilicate honeycomb primary mirrors.





Spinning furnace casts up to 8.4m mirrors as fast as f/1.1.

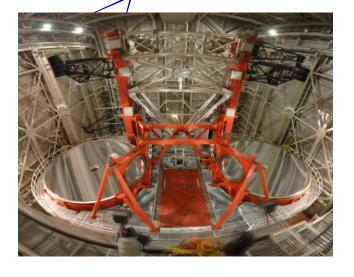
Highly aspheric mirrors are polished and tested after casting



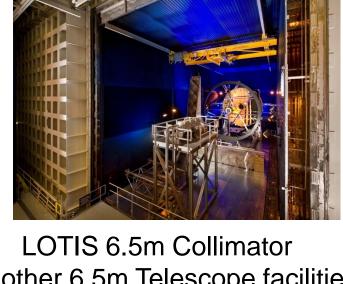
Projects with large borosilicate



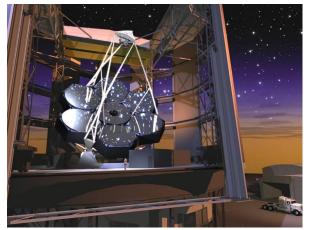




LBT: 2-8.4m mirrors



+ 4 other 6.5m Telescope facilities



GMT: 7-8.4m mirrors are part of a 25m f/0.7 parent. The first off-axis segment is cast and polishing is 80% completed.





4m Concept



Packaged into

existing Delta IV

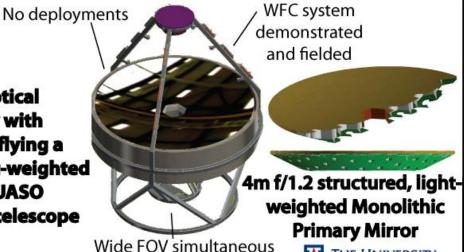
fairing



Reference Mission

NIIRS 7+ minimum performance with a goal of NIIRS 8
500km circular orbit
Simultaneous MWIR and visible TMA push broom
Metric imaging wavelength 600nm
Resolution more important than light gathering power
(therefore a large central obstruction is acceptable)

Replace optical complexity with simplicity by flying a downsized, light-weighted version of UASO ground-based telescope



THE UNIVERSITY

OF ARIZONA.

500 km circular orbit

Optical &

Detector

8μm pixels, 2 pixels per Airy disk, consider 2.5 pixels per Airy disk during Study 1.2° FOV, conduct a trade during Study

MWIR and visible

Requirements Field distortion less than 1/4 pixel across 64 pixels (1/8 Airy disk)

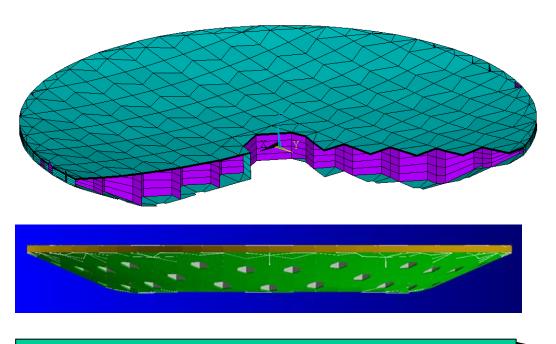




Steward Observatory Mirror Laboratory

Proposed high efficiency 4m casting for space





Specifications:

- 4m f/1.2
- Weight: 1188 kg
- Areal density: 95 kg/m²
- face/back plates: 12.7mm
- webs: 9.5mm thick
- 87 cells: 400mm diameter
- Contoured backplate
 - Stiffness x40 of equiv
 mass meniscus

Equivalent mass slab (1:100) 40mm thick

The above new type of casting is considered very low risk using heritage casting techniques, but is 1/7th the areal density of the mirrors previously cast by UASO.



Primary Mirror Comparison



Property	HST Spitzer JWST		UASO Flight qualified	Meniscus for flight ⁺	UASO ground	Hextek Gas Fusion	
Material	ULE	Be	Be	Ohara E6	ULE or Zerodur	Ohara E6	Borofloat
Diameter (m)	2.4	0.85	1.5 (seg)	4.0	4.0	8.4	Up to 1.5m
Temperature (K)	300	4	30	300	?	300	30 & 300
Surface figure (nm rms)	6.4	75	25	18 [†]	15 (typ)	18 (typ)	?
Areal Density (kg/m²)	180‡	28	26	95 ^{†‡}	220‡*	700	50‡
Areal Cost (\$M/m ²)							
(adjusted to 2008	21	13	6	3 †	?	0.4	?
dollars)							

[†] Estimates to be refined with future work.

Comparison of finished primary mirror optics. We estimate the cost of a finished flight-qualified 4m UASO mirror to be approximately 6-7 times the areal cost of a typical UASO mirror produced for ground-based telescopes. The added cost includes refined flaw detection and removal, enhanced treatments of as-cast surfaces, new mold designs, and dynamic and thermal TRL demonstrations. All areal costs adjusted to 2008.



^{*} Meniscus (1:40).

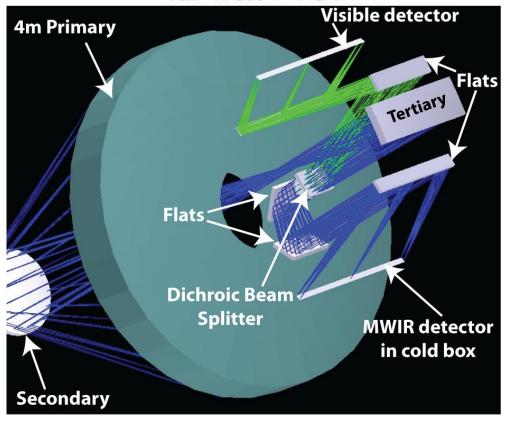
[‡] includes substrate only.



Notional surveillance instrument Very large and well-suited to LEO



f/18 Telescope Strawman Design Simultaneous MWIR & Visible Push Broom 1.2° x 0.04° FOV

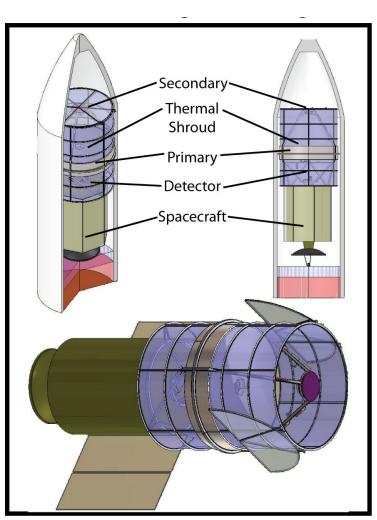


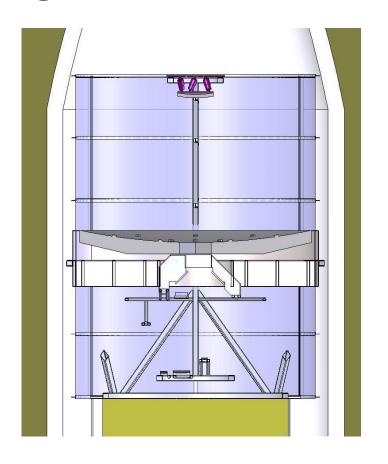




EELV Packaging for Launch







Crossection of telescope and instrument. Volume is within shroud keep-out zone.





CBE Mass Table



Mass with pre-Phase A margin shows ~0.5 mT remaining capacity

- No light-weighting measures have been applied except for primary mirror
- Many details have not been included except as placeholders

P/L element	Unit Mass (lbs)	Unit mass (mT)	
pacecraft (LMC)	20,000	9.091	_
Telescope			
Model			
18889 4M Primary Monolithic Mirror	2,500	1.136	
Monolith Secondary Mirror	90	0.041	
18891 4M Space Telescope Cell	2,500	1.136	
Rectangular Mirror One	110	0.050	
Mirror Assembly Frame	3,700	1.682	
Rectangular Mirror Two	20	0.009	
Rectangular Mirror Four	12	0.005	
Rectangular Mirror Five	20	0.009	
Rectangular Mirror Three	20	0.009	
Rectangular Mirror Six	28	0.013	
Rectangular Filter	30	0.014	
Pps Assemblies	90	0.041	
Sleeve	1,300	0.591	
Monolith Lid	800	0.364	
Hexapod	200	0.091	
Other elements			
Hardpoints	22	0.010	
Primary mirror actuators	11	0.005	
WCSS	440	0.200	
Secondary			
Secondary cell	90	0.041	
Wavefront monitoring system			
Hartmann mirror system	1	0.001	
Shack-Hartmann at ISS	22	0.010	
Focal plane detector	1,320	0.600	
Thermal management			
Blankets	176	0.080	
Deployments			
Active system	220	0.100	
Telescope control electronics			
Power supply	11	0.005	
Thermal monitoring	2	0.001	
Computer	11	0.005	
Interfaces			
Mechanical interface	44	0.020	
Cables	110	0.050	
Launch restraints	110	0.050	

		mT (metric t	ons)			
Unit Mass (lbs)	Unit mass (mT)	Quantity	Mass (CBE)	Margin	Current estimate	Basis	Note
20,000	9.091	1	9.09	10%	10.00	LMC 5/6/08	
2,500	1.136	1	1.14	30%	1.48	UASO model 6/4/08	Light-weighted E6
90	0.041	1	0.04	30%		UASO model 6/4/08	ULE solid
2,500	1.136	1	1.14	30%	1.48	UASO model 6/4/08	Steel
110	0.050	1	0.05	30%	0.07	UASO model 6/4/08	ULE solid
3,700	1.682	1	1.68	30%	2.19	UASO model 6/4/08	Steel
20	0.009	1	0.01	30%	0.01	UASO model 6/4/08	ULE solid
12	0.005	1	0.01	30%	0.01	UASO model 6/4/08	ULE solid
20	0.009	1	0.01	30%	0.01	UASO model 6/4/08	ULE solid
20	0.009	1	0.01	30%	0.01	UASO model 6/4/08	ULE solid
28	0.013	1	0.01	30%	0.02	UASO model 6/4/08	ULE solid
30	0.014	1	0.01	30%	0.02	UASO model 6/4/08	
90	0.041	1	0.04	30%	0.05	UASO model 6/4/08	
1,300	0.591	1	0.59	30%	0.77	UASO model 6/4/08	Aluminum on steel frame
800	0.364	1	0.36	30%	0.47	UASO model 6/4/08	
200	0.091	1	0.09	30%	0.12	UASO model 6/4/08	
22	0.010	6	0.06	30%	0.08	Guess	
11	0.005		0.25	30%		Guess	
440	0.200	1	0.20	30%	0.26	Guess	
90	0.041	1	0.04	30%	0.05	Guess to equal SM	
						•	
1	0.001	36	0.02	30%		Guess	
22	0.010		0.01	30%	0.01	Guess	
1,320	0.600	1	0.60	30%	0.78	Guess	
176	0.080	1	0.08	30%	0.10	need placeholder	
				30%		need placeholder	
220	0.100	1	0.10	30%	0.13	need placeholder	
11	0.005	1	0.01	30%	0.01	SWAG	
2	0.001	1	0.00	30%		SWAG	
11	0.005	1	0.01	30%		SWAG	
44	0.020	1	0.02	30%		Guess	
110	0.050		0.05	30%		Guess	
110	0.050		0.05	30%	0.07	Guess	



19.20 Launch capacity

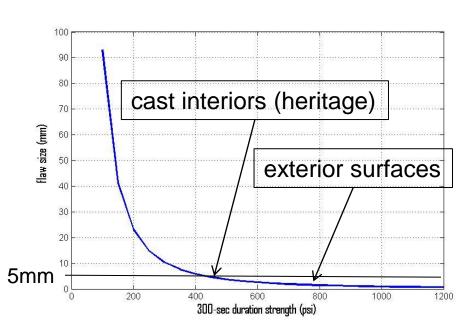
3.43 22% **3% 0.51** Net & reserve





Launch Survival of Primary: As-Cast E6 Flaws Affect Strength





- 300-sec duration strength (3σ) vs. flaw size in E6 as-cast. The 99% strength is 450 psi for 5mm flaw size. Further blank structure optimization and localized interior grinding will create significant improvements that guarantee launch and flight testing with ample margin.
- Exterior surfaces finished to 0.2mm
 flaws using standard procedures

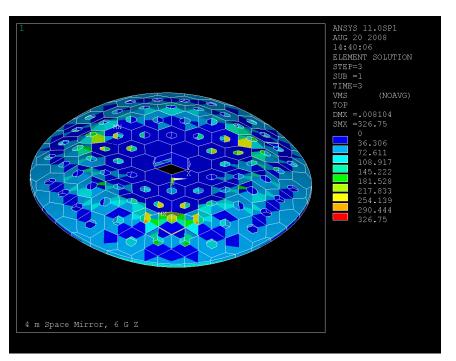
Current UASO casting procedures detect and repair all flaws down to 5mm (450 psi).

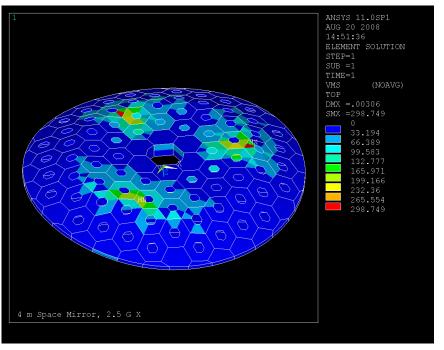




3-Point Support Stresses







Three-point stress distributions for 6gz (left) and 2.5 gx load cases. The total area of stress near 300 psi is small and can be further reduced through design. Bipod will have 6-pt contact, so survival has even more margin.

Analysis shows current UASO casting processes survive 3-point launch loads.

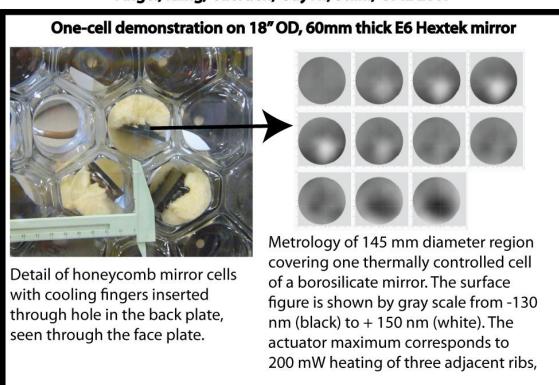




Using the glass CTE to advantage by thermal figuring the primary mirror



Angel, Kang, Cuerden, Guyon, Stahl; SPIE 2007



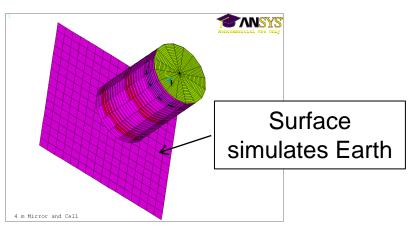
Previous work has shown that complete thermal figuring should be possible. Such figuring turns the borosilicate CTE into an advantage and could eliminate the need for instruments to provide a wavefront correction relay.

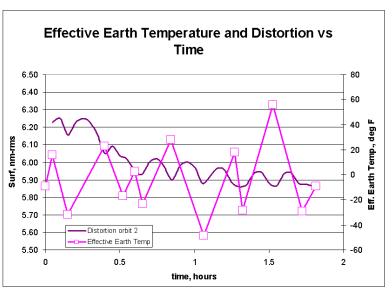




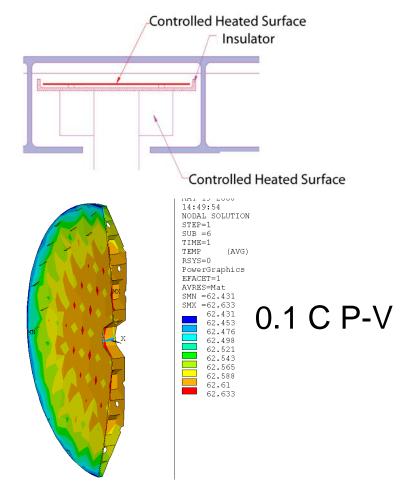
Thermal Figuring: Earth Looking with a sun-lit 290K thermal shroud







Each mirror cell contains a radiative heater with 2 zones

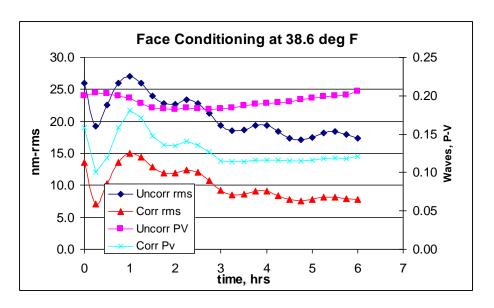


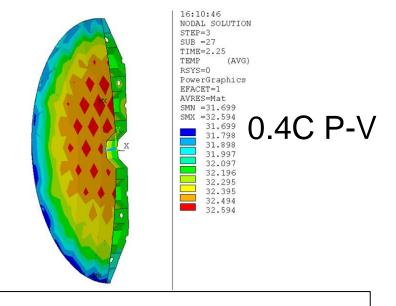


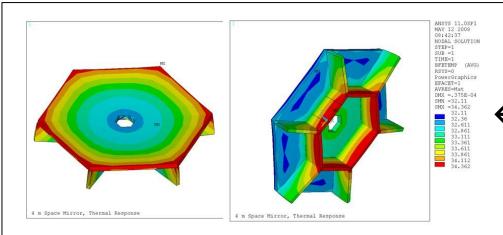


Thermal Figuring: Space-Looking with a sun-lit 270K thermal shroud









Thermal error distribution of each mirror cell might require another thermal zone to eliminate for space-looking.





Thermal conditioning conclusions



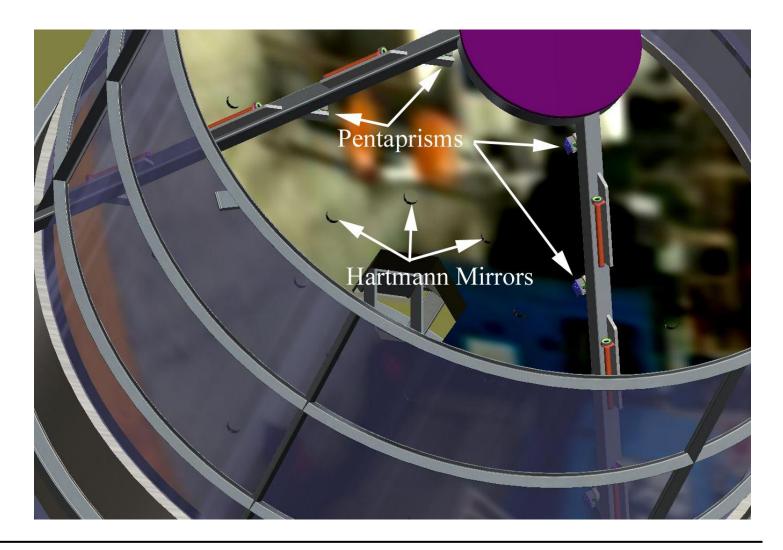
- Demonstrated good performance for earth-looking case including scene temperature changes and sun exposure with fixed set points so good figure is assured once the set points are established for the average conditions.
- Space-looking performance is not yet demonstrated for a highquality UV telescope (further analysis is needed).
- Heater set points appear to have a tolerance of 0.05 C which is an achievable level, particularly since they only have to be maintained to within that range once the set point is established.
- Additional temperature controlled zones can be added to further improve performance.
- Total thermal conditioning power estimates:
 - An e* = 0.008 shroud loses 350W to space, but gains 380W from solar heating, so balancing is needed (maybe via heat pipes)
 - When scene is 10C cooler than shroud, 30W is required increasing to 300W for space-looking.
 - 80W is required to equalize earth-shadow cases
 - Total power estimates: earth-looking ~ 110W, space-looking ~ 500W





Flight WFC Implementation on-orbit wavefront insurance policy



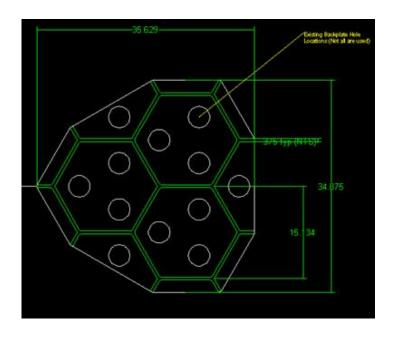




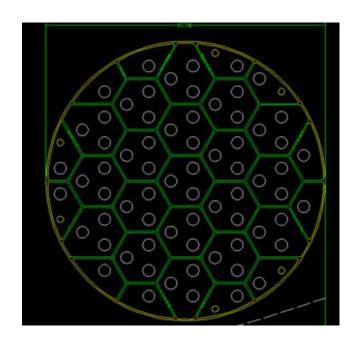


Upcoming work: casting mirrors with 95 kg/m² areal density





3-cell castings in small furnace for strength samples



2m diameter castings for TRL demonstrations of launch survival loads





Upcoming work: thermal figuring





We have a 1.8m mirror with a high quality sphere polished into it that will be used to test complete thermal mirror figuring.





Conclusions



- E6 borosilicate has been shown to be a credible primary mirror substrate material for space imaging applications.
- It's particularly well suited for earth-looking where the scene and shroud temperatures can be matched.
- Producing a high-quality space-looking telescope however requires more work to identify better thermal management schemes.
- The relatively high CTE of borosilicate has the potential to create thermal figuring solutions free of moving parts and relieving instruments of wavefront correction duties.
- Analysis shows high potential for cast structures to survive launch environment with good factors.
- Borosilicate is the only glass that can be cast in complex shapes. It has the potential to create cost-effective, low risk monolithic space imagers whose technology has already been proven at Ares V shroud diameters.

